



U.S. Department  
of Transportation  
**Federal Highway  
Administration**

June 28, 1995

400 Seventh St. S.W.  
Washington, D.C. 20590

Refer to: HNG-14

J. M. Essex, P.E.  
Vice President, Sales  
Energy Absorption Systems, Inc.  
One East Wacker Drive  
Chicago, Illinois 60601

Dear Mr. Essex:

Your March 1 letter to Mr. William A. Weseman referenced an earlier meeting you had with members of my staff, during which you provided videotapes and a written report documenting the National Cooperative Highway Research Program (NCHRP) Report 350 test level 3 (TL-3) performance of your Energite III (Sand Barrel) crash cushion. At that meeting, you requested that this office delay formal action on your request pending implementation of changes reflecting the metrication transition and of an educational campaign designed for the end-user of your product.

On May 30 you wrote to Mr. Weseman requesting the Federal Highway Administration (FHWA) to proceed with our review process and to respond to some specific issues addressed in that second letter.

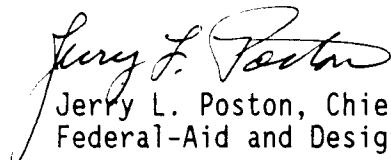
Each module in the Energite III array consists of a solid plastic barrel with a lid. The amount of sand placed in each barrel and its center of gravity are controlled by an inner cone that rests inside each of the three lightest weight modules. Based on some preliminary crash tests to evaluate the performance of an Energite III array per the NCHRP Report 350 matrix for a TL-3, non-redirective crash cushion, a 12-barrel standard array was selected for compliance testing. From front to back, the tested array consisted of one single 90-kg (200-pound) module, two rows of single 180-kg (400-pound) modules, one single 320-kg (700-pound) module, two rows of two 320-kg (700-pound) units, one row of two 640-kg (1400-pound) units, and finally, one row of two 960-kg (2100-pound) units. Each module was spaced approximately 150 mm to 200 mm apart, with the rear-most barrels at least 300 mm from the shielded object with a minimum 760-mm lateral offset from the corner of the hazard.

The NCHRP Report 350 tests 3-40 through 3-44 were conducted on the array described above. Test results are shown on the enclosed excerpts from the Energite III crash test report dated May 1994. The occupant risk measurements are summarized on Table C-1 from the report, which is also enclosed.

Based on the above noted test results, we concur with your finding that the Energite III array, as tested, fully meets the NCHRP Report 350 requirements for a TL-3 non-redirective crash cushion and it may continue to be used on the National Highway System (NHS) when selected by a highway agency. All requirements pertaining to the use of a proprietary product on federally-funded projects (except exempt non-NHS projects) remain in effect. By a copy of this letter, we will inform our field offices of this determination.

Two other items addressed in your May 30 letter concerned the selection of a design procedure that will address the multiple test level designations contained in the NCHRP Report 350 and FHWA's current position on the use of single-row sand barrels in work zones. We believe it appropriate to address both of these concerns in a separate letter and we will do so in the near future.

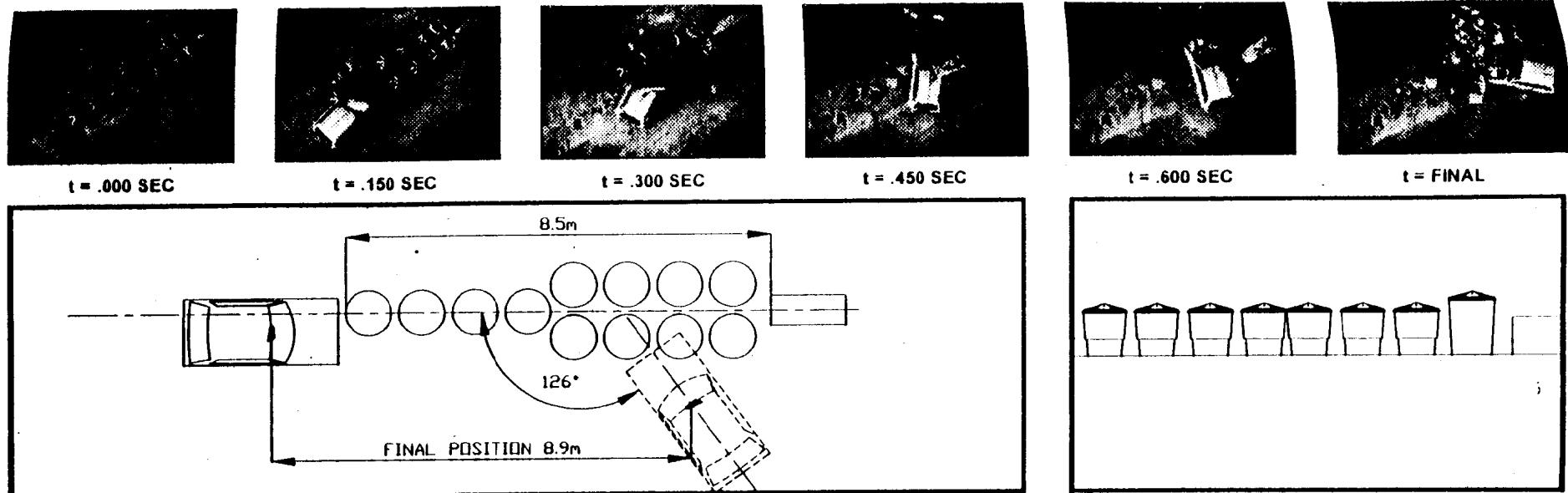
Sincerely yours,



Jerry L. Poston  
Chief  
Federal-Aid and Design Division

2 Enclosures

Geometric and Roadside Design Acceptance Letter CC-29



#### General Information

Test No. .... 177-011  
Date ..... Jan 10, 1994

#### Test Article

Type ..... Energié III  
Installation Length (m) ..... 8.5  
Size and/or dimension and material  
of key elements..... N/A

Soil Type and Condition ..... Clean Dry PCC

Test Vehicle  
Type ..... Production Model  
Designation ..... 820C  
Model ..... 1988 Ford  
Festiva

Mass (kg)  
Curb ..... 762  
Test inertial ..... 818  
Dummy(s) ..... 75  
Gross Static ..... 893

Impact conditions  
Speed (km/h) ..... 100.5  
Angle (deg)..... 0  
Impact Severity (kJ) ..... 319.1

#### Exit conditions

Speed (km/h) ..... N.A  
Angle (deg)..... N/A

#### Occupant Risk Values

Impact Velocity (m/s)	
x-direction	7.99
y-direction	0.06
Ridedown Acceleration (g's)	
x-direction	-12.46
y-direction	-6.30

Acceleration Severity Index ..... 0.77

#### Test Article Deflection (m)

Dynamic	N/A
Permanent	N/A

#### Vehicle Damage

Exterior	
VDS	FD-5
CDC	I2FDEW5

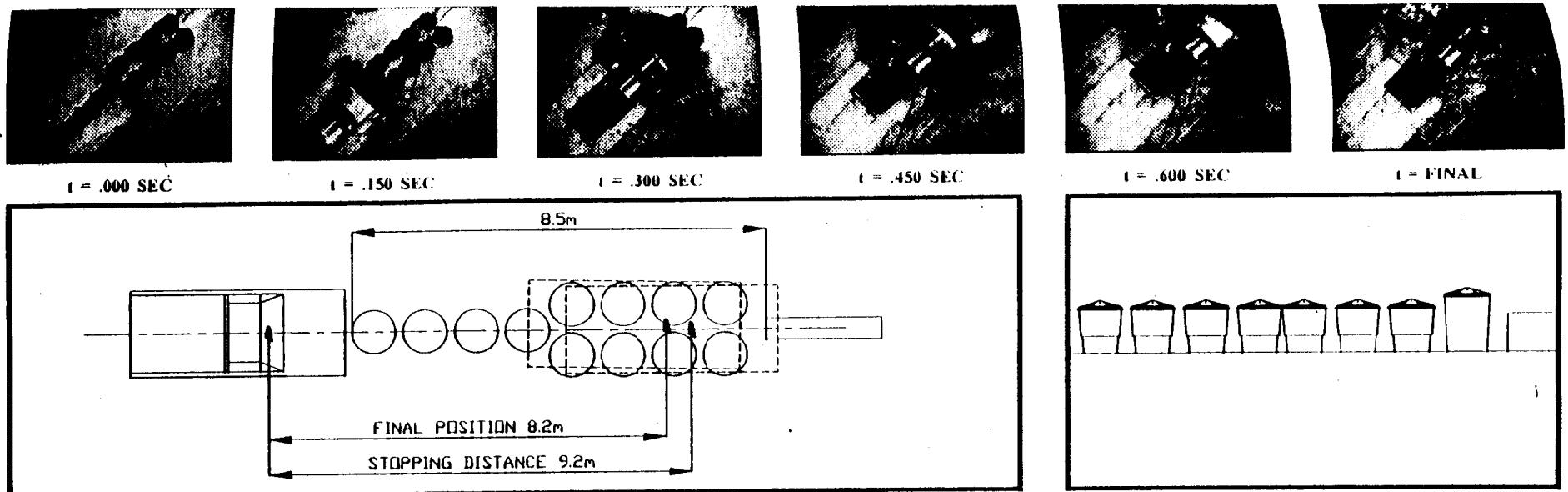
#### Interior

OCDL	AS0000000
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#### Post-Impact Vehicular Behavior

Maximum Roll Angle (deg)	-12.5
Maximum Pitch Angle (deg)	-5.3
Maximum Yaw Angle (deg)	-126.3

Figure 1. Summary of Results - Energié III Test 177-011  
(NCHRP 350 Test 3-40)



#### General Information

Test No. .... 177-015  
Date ..... April 22, 1994

#### Test Article

Type ..... Enercite III  
Installation Length (m) ..... 8.5  
Size and/or dimension and material  
of key elements..... N/A

#### Soil Type and Condition

Clean Dry PCC  
Test Vehicle  
Type ..... Production Model  
Designation ..... 2000P  
Model ..... 1988 GMC  
Sierra 2500

Mass (kg)  
Curb ..... 1923

Test inertial ..... 2005

Dummy(s) ..... N/A

Gross Static ..... 2005

#### Impact conditions

Speed (km/h) ..... 102.8

Angle (deg)..... 0

Impact Severity (kJ)..... 817.1

#### Exit conditions

Speed (km/h) ..... N/A  
Angle (deg) ..... N/A

#### Occupant Risk Values

Impact Velocity (m/s)	
x-direction	7.96
y-direction	0.01
Ridedown Acceleration (g's)	
x-direction	-14.22
y-direction	3.06
Acceleration Severity Index	0.69

#### Test Article Deflection (m)

Dynamic	N/A
Permanent	N/A

#### Vehicle Damage

Exterior	
VDS	FD-4
CDC	12FDEW4

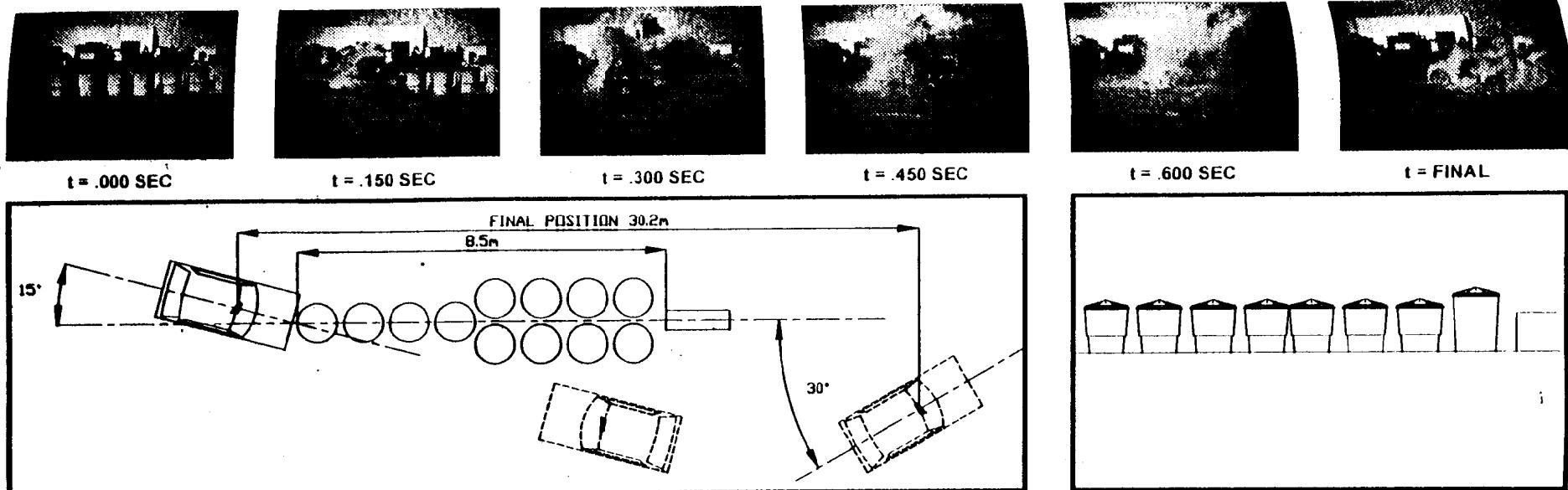
#### Interior

OCDL	AS0000000
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#### Post-Impact Vehicular Behavior

Maximum Roll Angle (deg)	-2.4
Maximum Pitch Angle (deg)	-5.2
Maximum Yaw Angle (deg)	3.5

Figure 6. Summary of Results - Enercite III Test 177-015  
(NCHRP 350 Test 3-41)



#### General Information

Test No. .... 177-006  
Date ..... Sept. 22, 1993

#### Test Article

Type ..... Energeite III  
Installation Length (m) ..... 8.5  
Size and/or dimension and material  
of key elements..... N.A.

Soil Type and Condition ..... Clean Dry PCC

#### Test Vehicle

Type ..... Production Model  
Designation ..... 820C  
Model ..... 1987 Honda  
..... Civic

Mass (kg)  
Curb ..... 853  
Test Inertial ..... 843  
Dummy(s)..... 75  
Gross Static ..... 918

#### Impact Conditions

Speed (km/h) ..... 103.0  
Angle (deg) ..... 15  
Impact Severity (kJ) ..... 345.1

#### Exit conditions

Speed (km/h) ..... 42.8  
Angle (deg) ..... 30

#### Occupant Risk Values

Impact Velocity (m/s)  
x-direction ..... 7.00  
y-direction ..... 0.24  
Ridedown Acceleration (g's)  
x-direction ..... -12.98  
y-direction ..... -8.15

Acceleration Severity Index ..... 0.71

#### Test Article Deflection (m)

Dynamic ..... N.A.  
Permanent ..... N.A.

#### Vehicle Damage

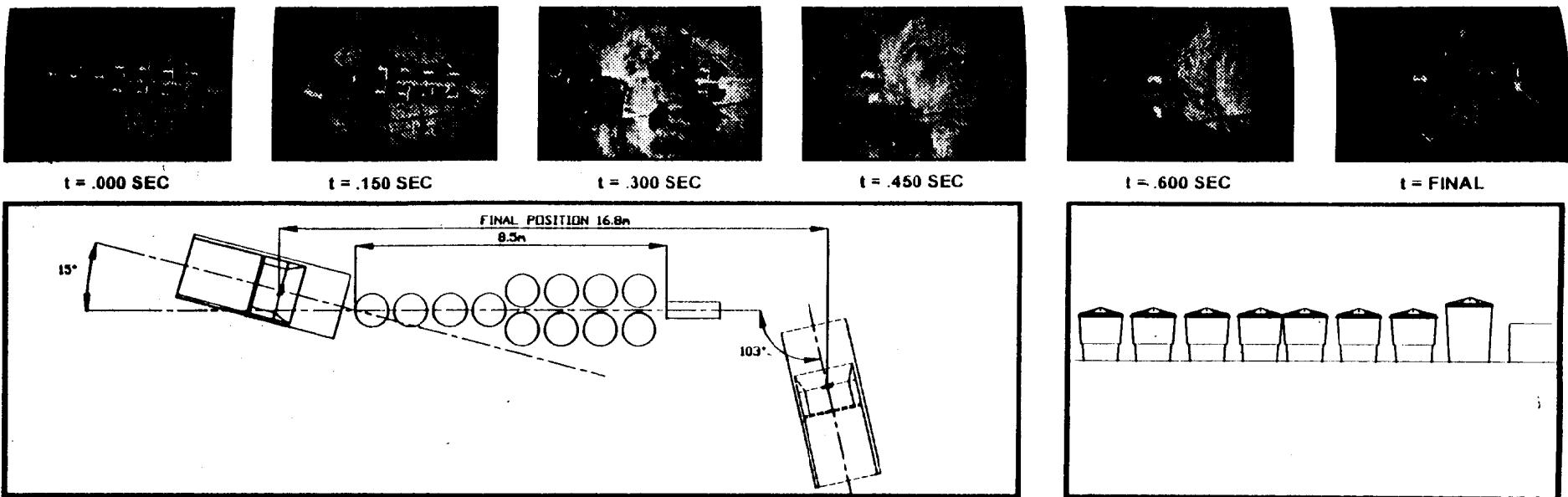
Exterior  
VDS ..... FL-4  
CDC ..... 11FYAW6

Interior  
OCDI ..... AS0000000

#### Post-Impact Vehicular Behavior

Maximum Roll Angle (deg) ..... 7.0  
Maximum Pitch Angle (deg) ..... -7.4  
Maximum Yaw Angle (deg) ..... -180.3

Figure 11. Summary of Results - Energeite III Test 177-006  
(NCHRP 350 Test 3-42)



#### General Information

Test No. .... 177-005  
Date ..... Sept. 15, 1993

#### Test Article

Type ..... Energete III  
Installation Length (m) ..... 8.5  
Size and/or dimension and material  
of key elements ..... N.A.

Soil Type and Condition ..... Clean Dry PCC

#### Test Vehicle

Type ..... Production Model  
Designation ..... 2000P  
Model ..... 1988 Chevrolet  
..... Cheyenne

#### Mass (kg)

Curb ..... 1855

Test Inertial ..... 2016

Dummy(s) ..... N.A.

Gross Static ..... 2016

#### Impact Conditions

Speed (km/h) ..... 101.9

Angle (deg) ..... 15

Impact Severity (kJ) ..... 807.9

#### Exit conditions

Speed (km/h) ..... 53.5  
Angle (deg) ..... 6

#### Occupant Risk Values

Impact Velocity (m/s)

x-direction ..... 6.51

y-direction ..... 0.47

#### Ridedown Acceleration (g's)

x-direction ..... -9.02

y-direction ..... 6.45

Acceleration Severity Index ..... 0.52

#### Test Article Deflection (m)

Dynamic ..... N.A.

Permanent ..... N.A.

#### Vehicle Damage

##### Exterior

VDS (primary / secondary) ..... FL-5 / RFQ-6

CDC (primary / secondary) ..... 11FYAWS / 01FZAW6

##### Interior

OCDI (primary / secondary) ..... AS0000000 / RF0012000

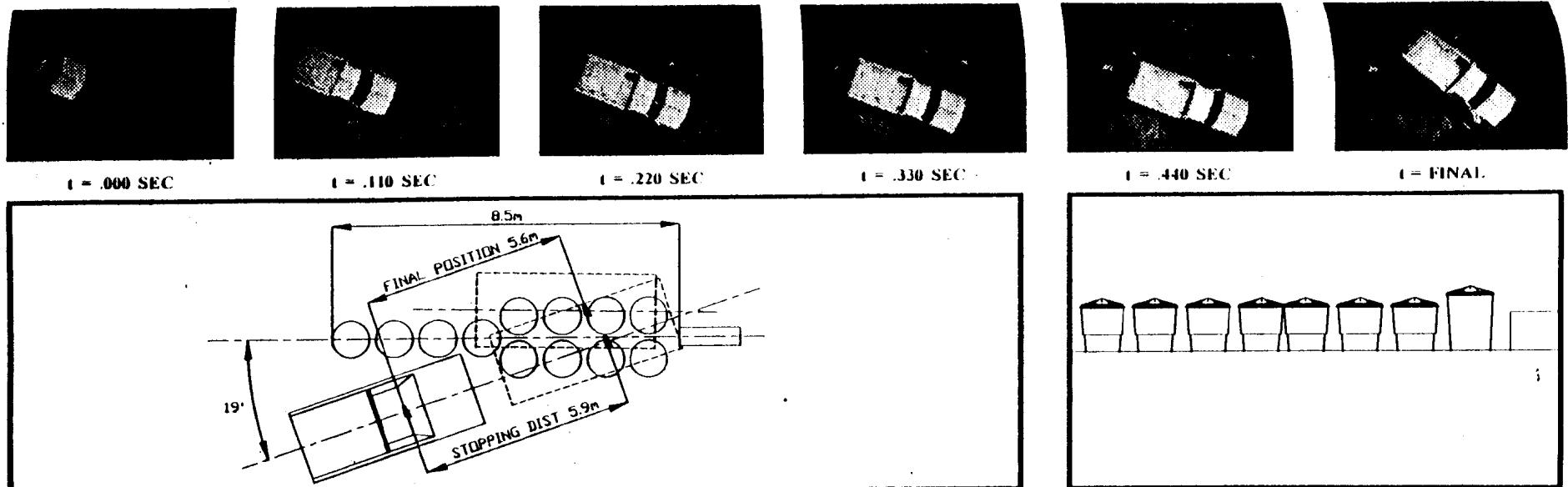
#### Post-Impact Vehicular Behavior

Maximum Roll Angle (deg) ..... -3.4

Maximum Pitch Angle (deg) ..... -8.1

Maximum Yaw Angle (deg) ..... -118.3

Figure 16. Summary of Results - Energete III Test 177-005  
(NCHRP 350 Test 3-43)



#### General Information

Test No. .... 177-016  
Date ..... May 4, 1994

#### Test Article

Type ..... Enercite III  
Installation Length (m) ..... 8.5  
Size and/or dimension and material  
of key elements ..... N/A

Soil Type and Condition ..... Clean Dry PCC

#### Test Vehicle

Type ..... Production Model  
Designation ..... 2000P  
Model ..... 1990 GMC  
..... 3/4 ton P/U

Mass (kg)  
Curb ..... 1950  
Test inertial ..... 1964  
Dummy(s) ..... N/A  
Gross Static ..... 1964

#### Impact conditions

Speed (km/h) ..... 96.5  
Angle (deg) ..... 19  
Impact Severity (kJ) ..... 705.3

#### Exit conditions

Speed (km/h) ..... N/A  
Angle (deg) ..... N/A

#### Occupant Risk Values

Impact Velocity (m/s)	
x-direction	9.71
y-direction	0.54
Ridedown Acceleration (g's)	
x-direction	-14.13
y-direction	-9.75

Acceleration Severity Index ..... 0.86

#### Test Article Deflection (m)

Dynamic	N/A
Permanent	N/A

#### Vehicle Damage

Exterior	
VDS	FD-5
CDC	12FDEW4
Interior	
OCDI	AS0000000

#### Post-Impact Vehicular Behavior

Maximum Roll Angle (deg)	-12.4
Maximum Pitch Angle (deg)	-4.4
Maximum Yaw Angle (deg)	17.2

Figure 21. Summary of Results - Enercite III Test 177-016  
(NCHRP 350 Test 3-44)

eled either 0.6 m forward or 0.3 m lateral, whichever is smaller. The flail space time was determined by incremental integration of the vehicular acceleration. The acceleration in the x direction was integrated twice with respect to time to find the flail space time at which the double integration equals 0.6 m. Acceleration in the y direction was integrated twice with respect to time to find the flail space time at which the double integration equals 0.3 m. Finally, a 10 ms moving average of the x and y vehicular accelerations were taken, and the ridedown accelerations were reported as the highest 10 ms average vehicular accelerations in the x and y directions subsequent to the flail space time.

The Acceleration Severity Index (ASI) was calculated according to the procedures contained in

NCHRP 350 Section F3.1. A 50 ms moving average of the x, y, and z vehicular accelerations are taken and then normalized by dividing by their repective limit accelerations (12, 9, and 10 g's, respectively). These values were then squared and summed, and the ASI was computed as a function of time as the square root of this sum. Occupant risk is assumed to be proportional to the maximum value of the ASI.

Table C-1 contains a summary of the occupant impact velocity, ridedown accelerations, and acceration severity index for Energite III Tests 177-011, 177-015, 177-006, 177-005, and 177-016. The vehicle angular displacements, longitudinal, lateral, and vertical g-trace and occupant kinematics, 10ms average vehicle accelerations, and ASI plots for these tests are shown in Figure C-3 through C-32.

Table C-1. Summary of Energite III Occupant Risk Measurements

NCHRP 350 Test Number	EASI Test Number	Flail Space Velocity		Ridedown Acceleration		Acceleration Severity Index
		Longitudinal	Lateral	Longitudinal	Lateral	
3-40	177-011	7.99 m/s @ 0.145 s	0.06 m/s @ 0.145 s	-12.46 g's @ 0.174 s	-6.30 g's @ 0.312 s	0.77 @ 0.214 s
3-41	177-015	7.97 m/s @ 0.164 s	0.02 m/s @ 0.164 s	-14.26 g's @ 0.347 s	3.06 g's @ 0.230 s	0.69 @ 0.219 s
3-42	177-006	7.00 m/s @ 0.151 s	0.24 m/s @ 0.151 s	-12.98 g's @ 0.286 s	-8.15 g's @ 0.224 s	0.71 @ 0.298 s
3-43	177-005	6.51 m/s @ 0.179 s	0.47 m/s @ 0.179 s	-9.02 g's @ 0.264 s	6.45 g's @ 0.252 s	0.52 @ 0.271 s
3-44	177-016	9.71 m/s @ 0.138 s	0.54 m/s @ 0.138 s	-14.13 g's @ 0.205 s	-9.75 g's @ 0.414 s	0.86 @ 0.245 s